# Challenges in Design and Construction of Deep Excavation for SEAGC 2018

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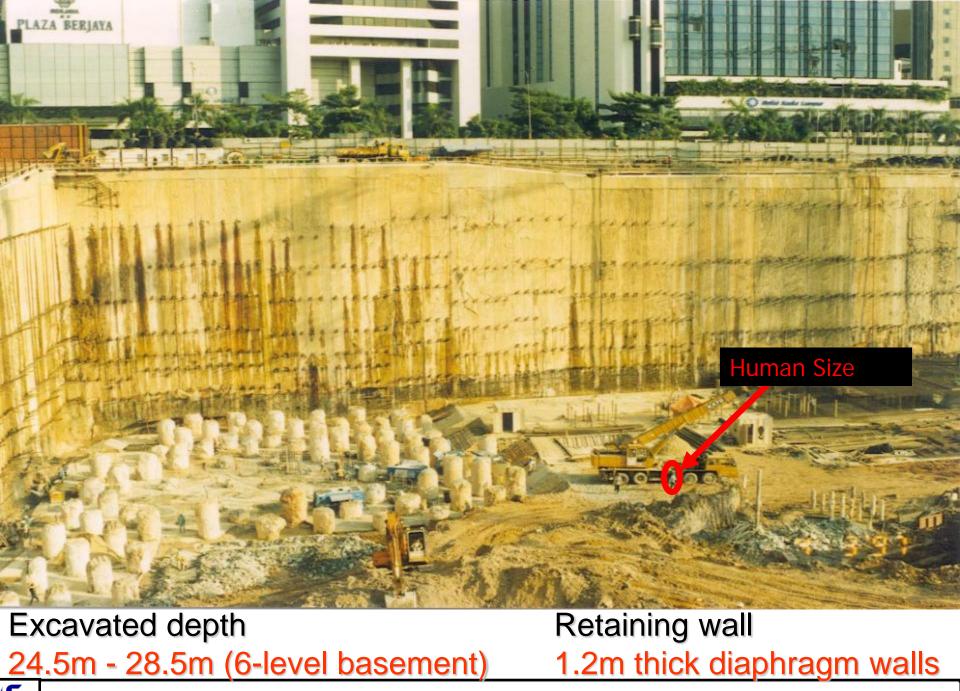
Date: 6th Nov 2018

### CONTENTS

- Introduction
- Design Considerations
  - Soil Parameters
  - Numerical Analyses
- Case Studies
  - Limestone
  - Circular shafts
  - Alluvium with high groundwater table
- Summary

- Deep basement construction
  - Urban areas for parking space
  - Infrastructures, e.g. MRT

 High Risk associated with deep basement construction!



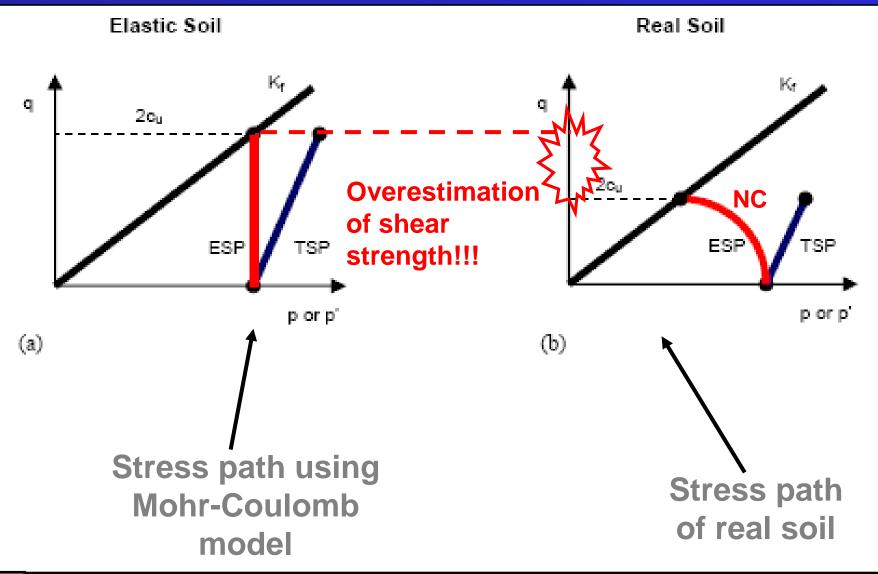
#### **FAILURES of DEEP EXCAVATION**



#### **FAILURES of DEEP EXCAVATION**







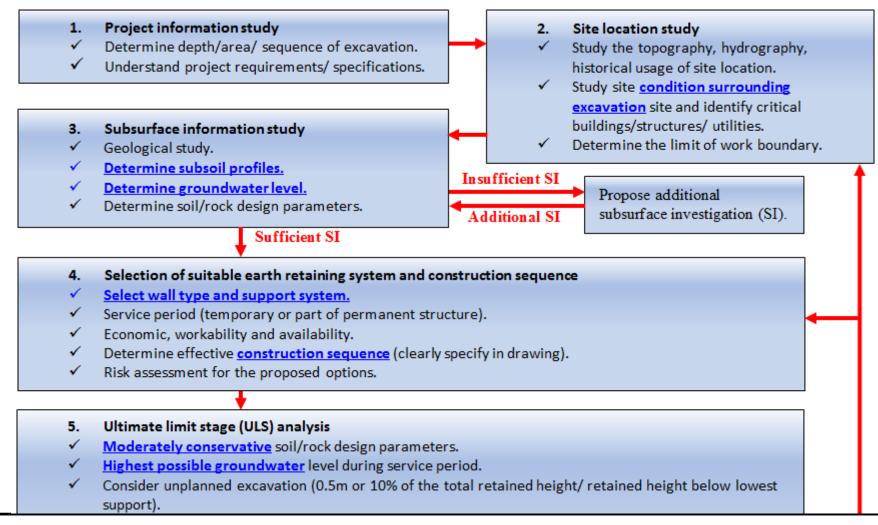




### **Common questions in Deep Excavation:**

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What are the parameters involved ?
         What are the pitfalls ?
   How to avoid failures ?
     Which temporary earth retaining
               system to use?
```

#### **Design Flowchart for Excavation Works**



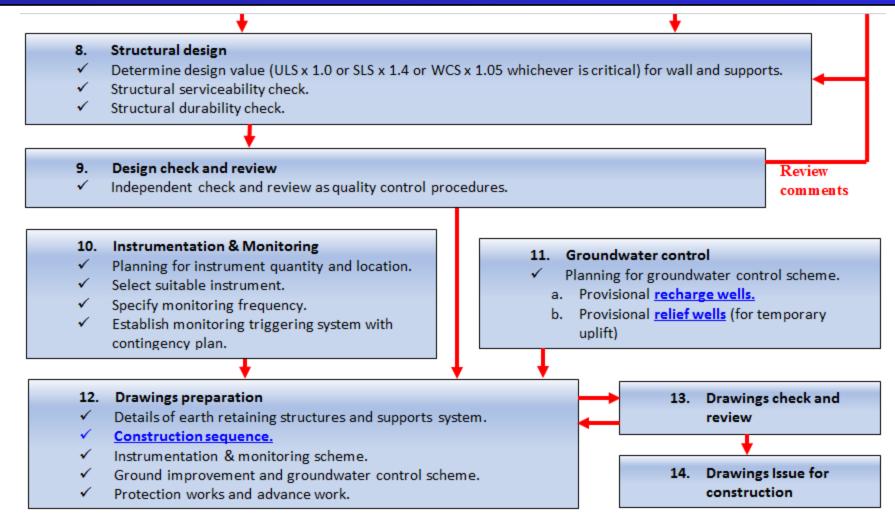
- 5. Ultimate limit stage (ULS) analysis
- Moderately conservative soil/rock design parameters.
- ✓ Highest possible groundwater level during service period.
- ✓ Consider unplanned excavation (0.5m or 10% of the total retained height/ retained height below lowest support).
- ✓ Surcharge load (construction/operational load or minimum 10kPa).
- ✓ Determine wall depth and support levels for following checks:
  - Wall stability check
  - Vertical stability check
  - Basal heave stability check
  - Hydraulic failures check
- Calculate wall bending moment, shear force and support load (ULS)

#### 6. Serviceability limit stage (SLS) analysis

- ✓ Moderately conservative soil/rock design parameters.
- ✓ Highest possible groundwater level during service period.
- ✓ Surcharge load (construction/operational).
- ✓ Follow wall depth and support levels in ULS analysis.
- <u>Evaluate deformation</u> of retaining wall and retained ground.
- Carry out <u>damage assessment</u> of surrounding buildings, structures and utilities.
- Calculate wall deflection, bending moment, shear force and support load (SLS).

- 7. Worst case scenario (WCS) analysis
- ✓ One strut failure.
- Accidental impact load on strut.
- ✓ Flooded condition.
- Calculate wall bending moment, shear force and support load (WCS).



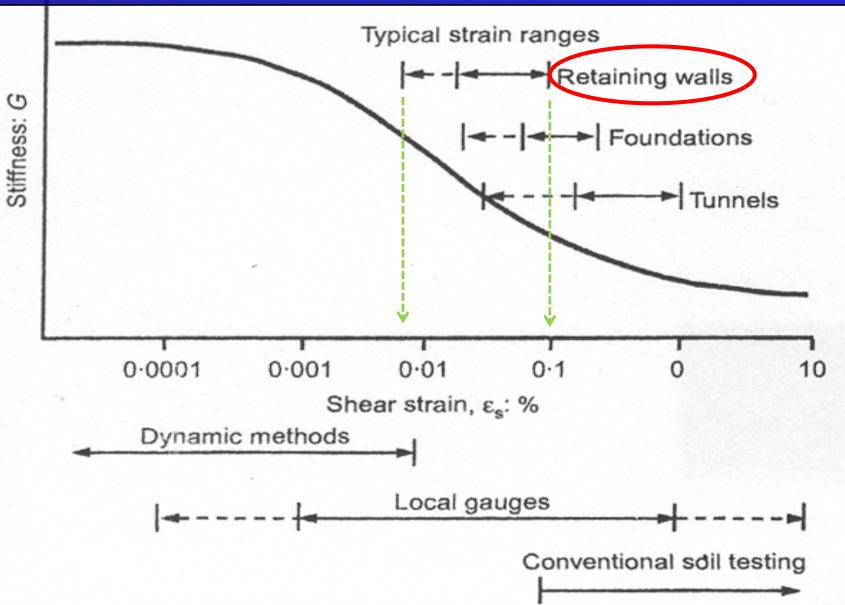




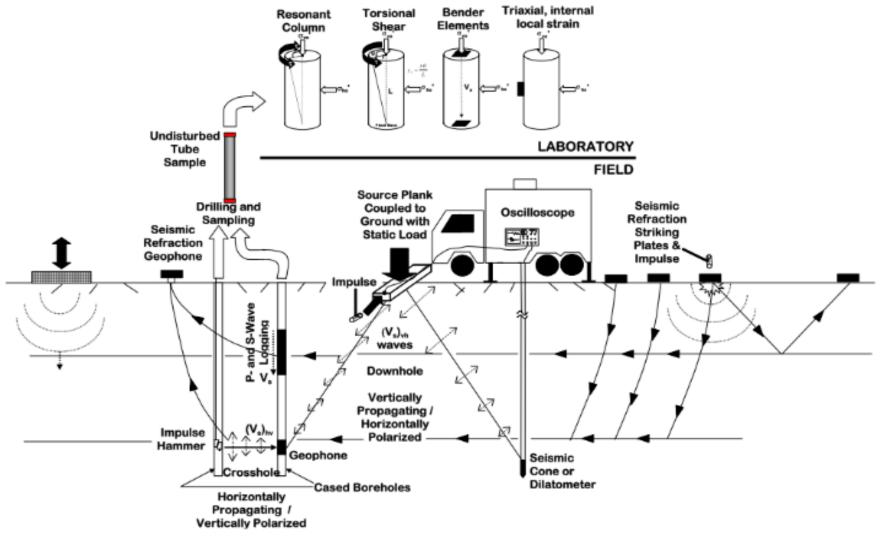
- Some important soil parameters related to retaining wall and support system design:
  - Shear strength parameters ( $s_u$ ,  $\phi' \& c'$ )
  - Soil permeability
  - Soil **stiffness**

### Soil stiffness

- Important parameters for retaining wall design BUT difficult to obtain reliably
- In Malaysia, pressuremeter, shear wave velocity and compare with empirical correlations
- Laboratory tests unreliable and values obtained significantly smaller than appropriate values for retaining wall design
- Designer should be aware of small-strain nature of retaining wall design



**G**&



Field and laboratory methods to evaluate shear wave velocity

Introduction – Design Considerations – Case Studies – Summary

**Typical values of maximum small-strain shear modulus** 

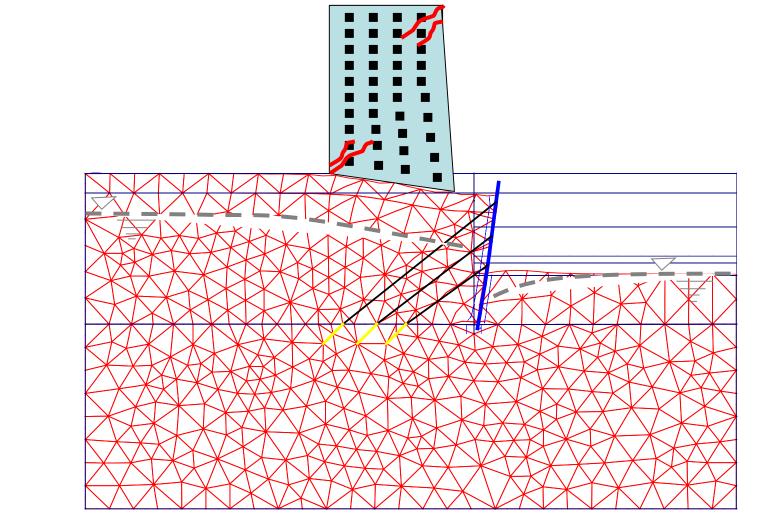
	Maximum small-strain shear modulus,		
Soil Type	G <sub>0</sub> (kPa)		
Soft clays	2,750 to 13,750		
Firm clays	6,900 to 34,500		
Silty sands	27,600 to 138,000		
Dense sands and gravels	69,000 to 345,000		

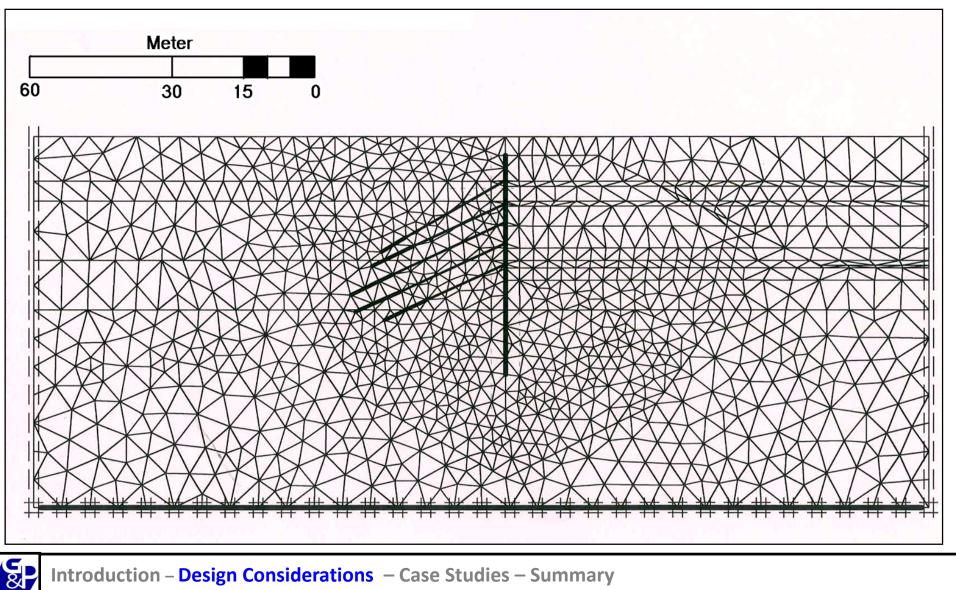
$$G_0 = 15,560 (N_{60})^{0.68}$$

$$G_0 = 1,634(q_c)^{0.25}(\sigma'_{vo})^{0.375}$$

$$\gamma_{0.7} = \frac{0.385}{4G_0} (2c(1 + \cos 2\emptyset) + \sigma'(1 + Ko) \sin 2\emptyset)$$

#### **GROUND MOVEMENT INDUCED BY DEEP EXCAVATION**





### **CONSTITUTIVE SOIL MODELS**

- Various constitutive soil models, e.g. Mohr-Coulomb, Cam Clay, Hardening Soil, Soft Soil, etc.
  - Proper understanding and limitations of each model important!
  - Incorrect use of soil models in Nicoll Highway!

### CASE STUDIES







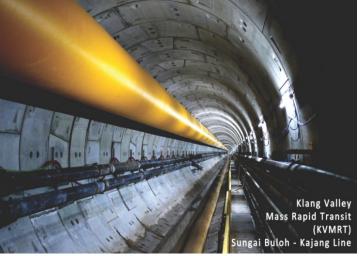


### **Case History 1:**

Deep Excavation for Three (3) Underground Stations for KVMRT in Limestone

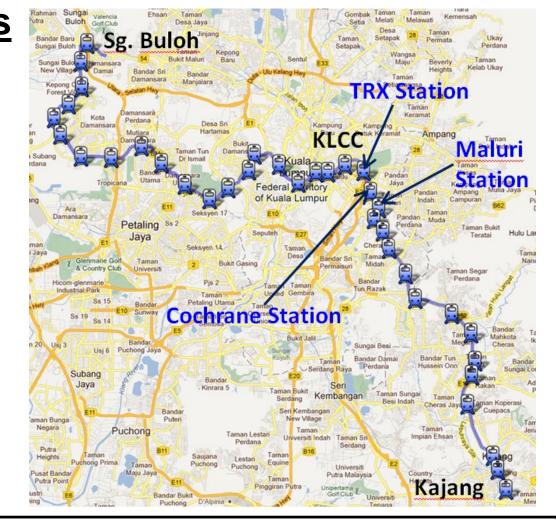
### - KVMRT Line 1, Sungai Buloh to Kajang





#### Locations of the MRT Underground

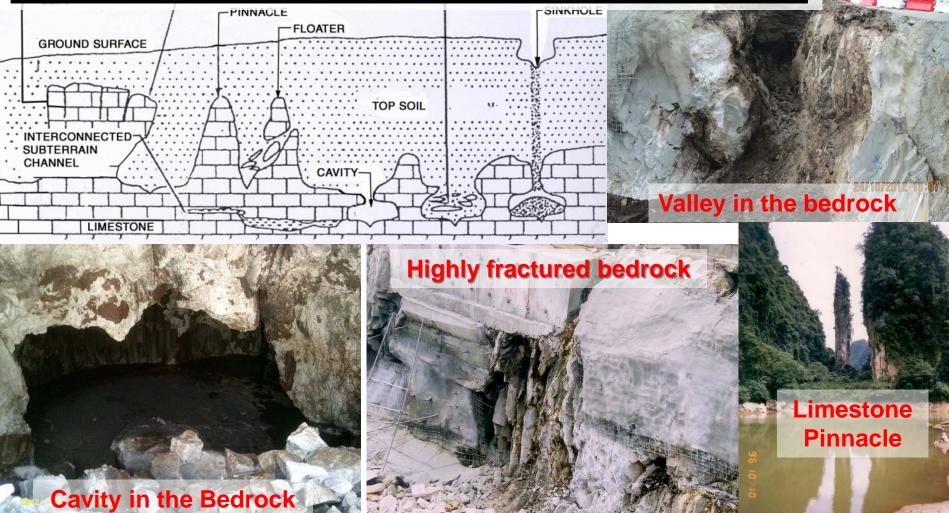
#### **Stations**



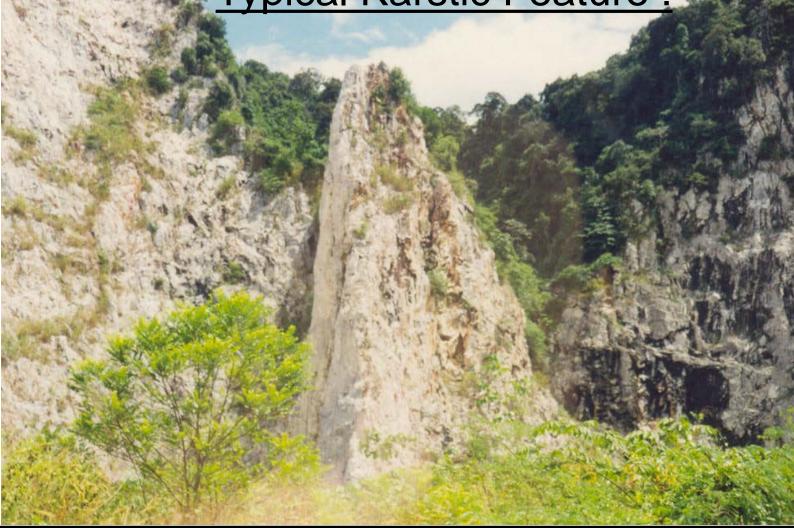
### **Geology of Kuala Lumpur**



#### Karstic Features of Kuala Lumpur Limestone

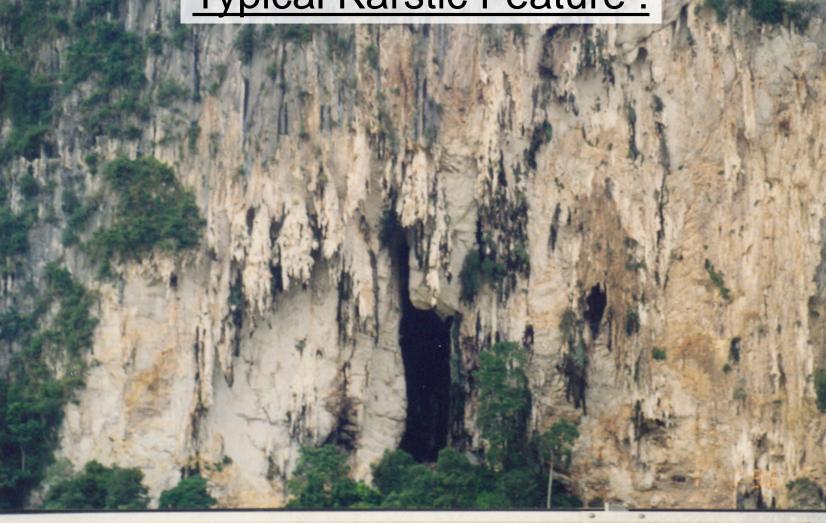






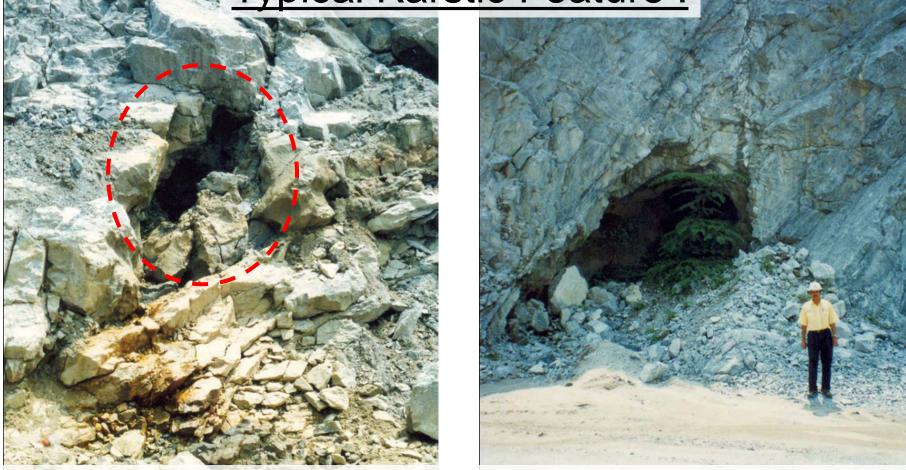


### **Typical Karstic Feature :**



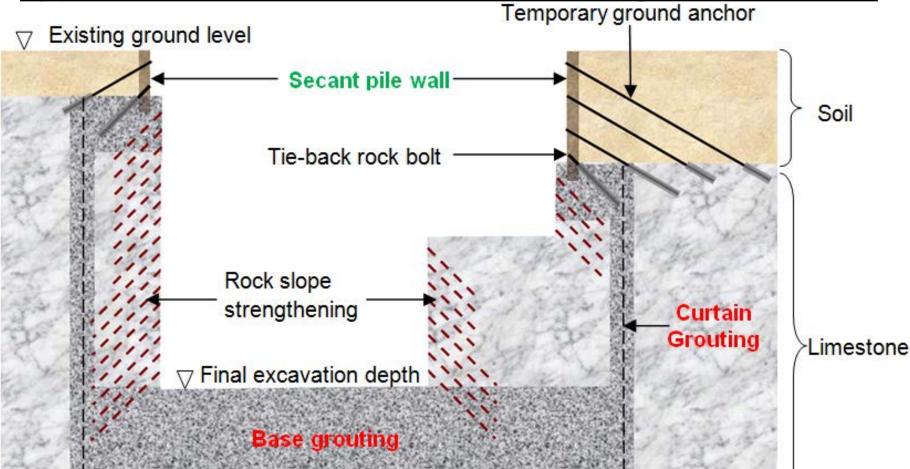


### **Typical Karstic Feature :**



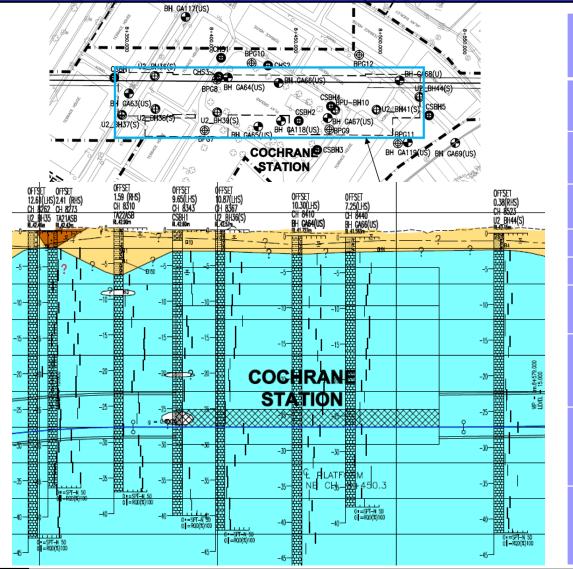
#### **CAVERN/CAVITY EXPOSED AFTER EXCAVATION**

#### **Typical Excavation Section for Underground Station**



(Note: Rock slope strengthening indicated is provisional only. Actual locations and extent of rock slope strengthening are determined after geological mapping works and kinematic analysis).

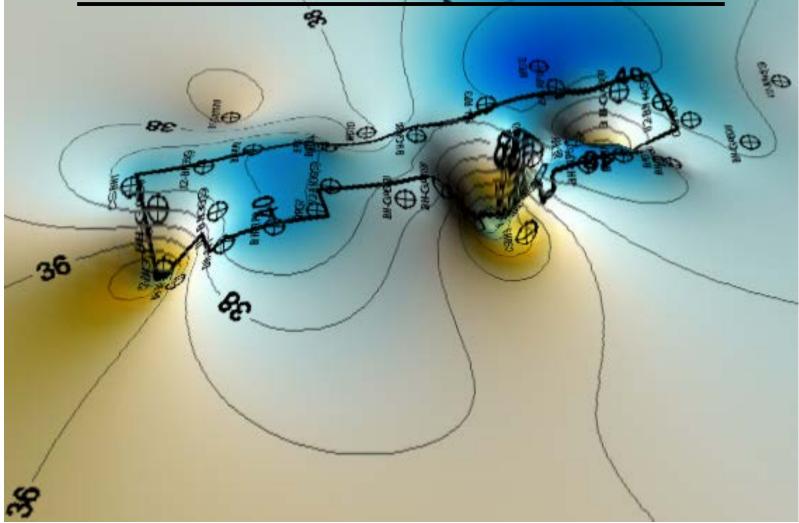




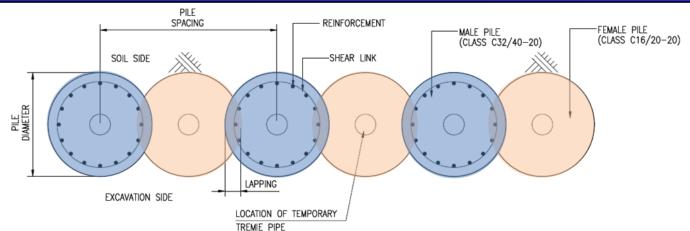
	Subsoil	Bedrock
Material type	Silty Sand	Limestone
Average depth	5m	5m below
Unit weight	18 kN/m <sup>3</sup>	24 kN/m <sup>3</sup>
SPT N	2 - 4	-
RQD	-	0 – 100%
Average UCS	-	50 MPa
Effective shear strength	c'= 1 kPa ¢'= 29°	c'= 400 kPa ¢'= 32°
Elastic Modulus, E' (kPa)	4000 - 12000	1.0E6 – 1.0E7
Hydraulic conductivity, k	1.0E-5 m/s	0 – 31 Lugeon

Introduction – Design Considerations – Case Studies – Summary

#### **Conchrane Station Bedrock Contour**

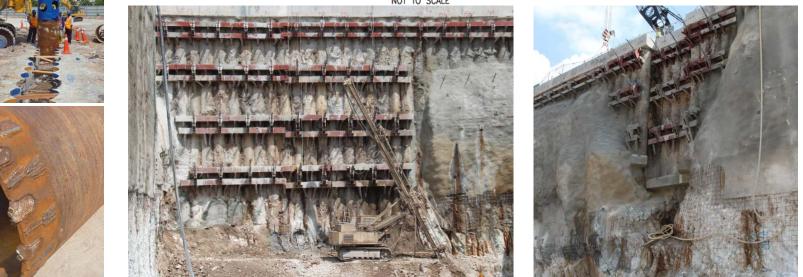






 TYPICAL CROSS SECTION OF TEMPORARY HARD/SOFT SECANT PILE WALL

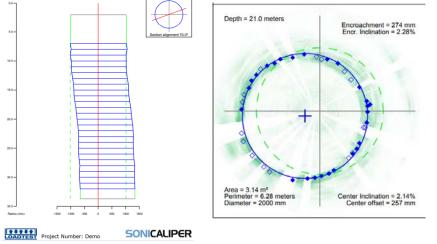
 (PLAN VIEW)





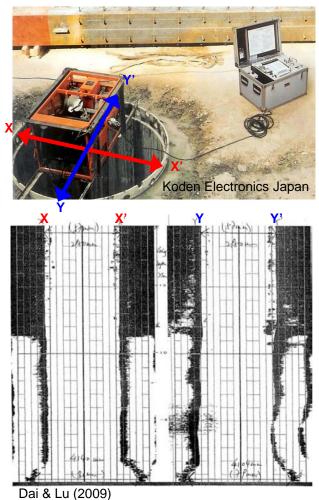
### Sonic Caliper





http://www.sonicaliper.com/soni/index.shtml

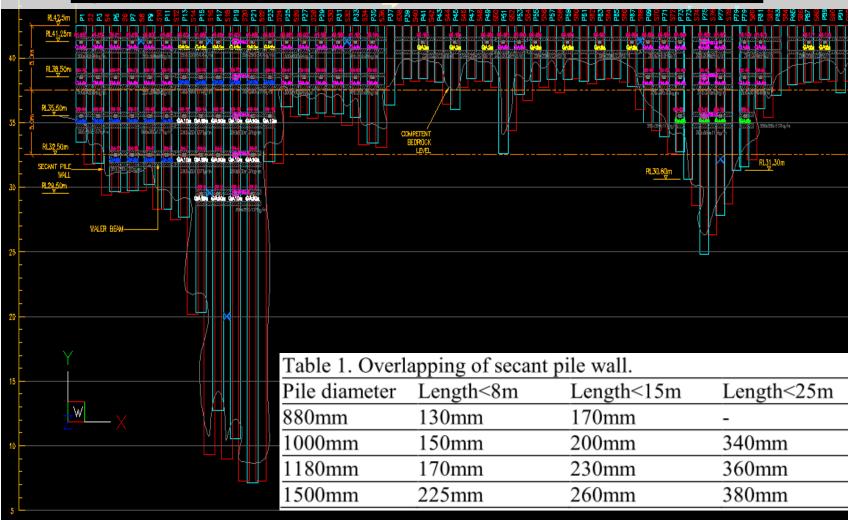
### Koden Test



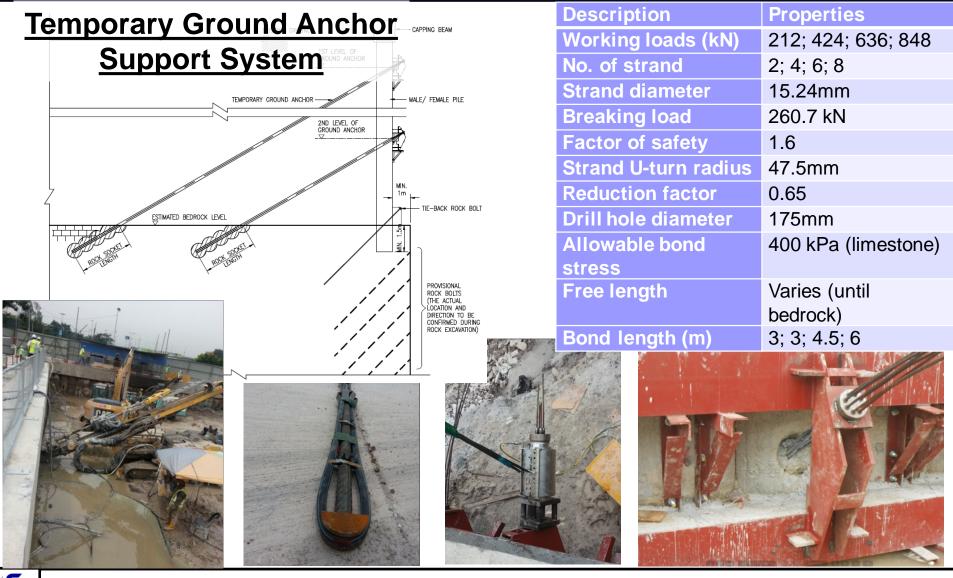


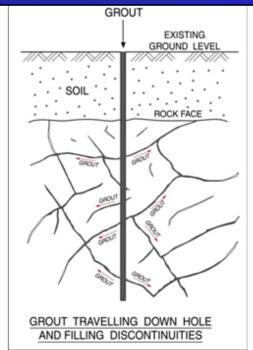
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### **Typical Secant Pile Wall Elevation View**









Curtain & Base Grouting to seal the Limestone Karstic Features



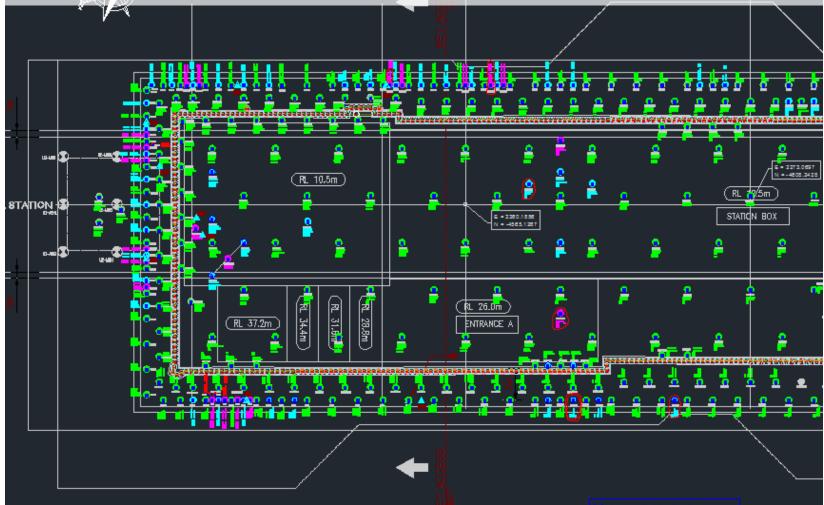
Table 3	. Holding	pressure	for	fissure	grouting
---------	-----------	----------	-----	---------	----------

	0 0
Depth (m)	Holding pressure (Bar)
0 to 10	2 to 4
10 to 20	6 to 8
20 to 30	10 to 12
30 to 40	14 to 16
40 to 50	18 to 20
>50	>22

Note: Termination criteria shall be satisfied with flow rate less than 2 liters per minute or grout volume reaches 10m<sup>3</sup> for every grouting zone in 5m depth.

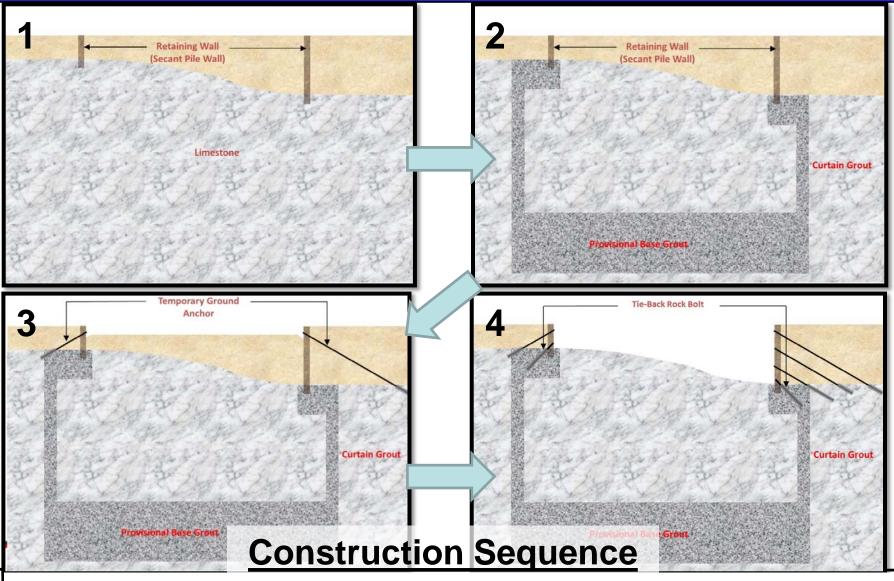


### **Typical Curtain & Base Grouting Holes Layout**



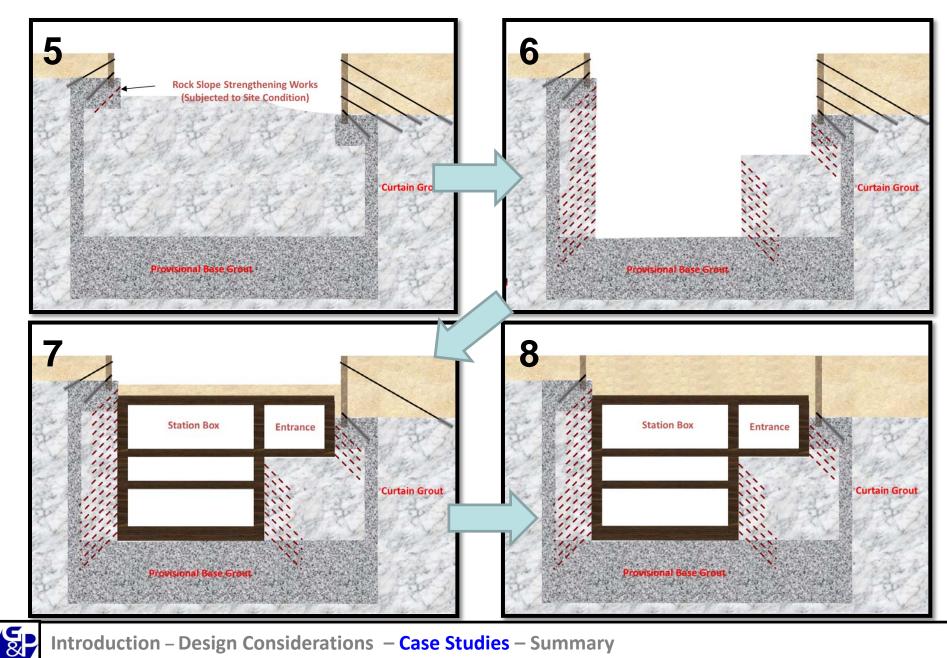
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CASE STUDIES - LIMESTONE



Introduction – Design Considerations – Case Studies – Summary

### **Constrution Sequence (con't)**



### **Exposed Vertical Rock Face of the Excavation**









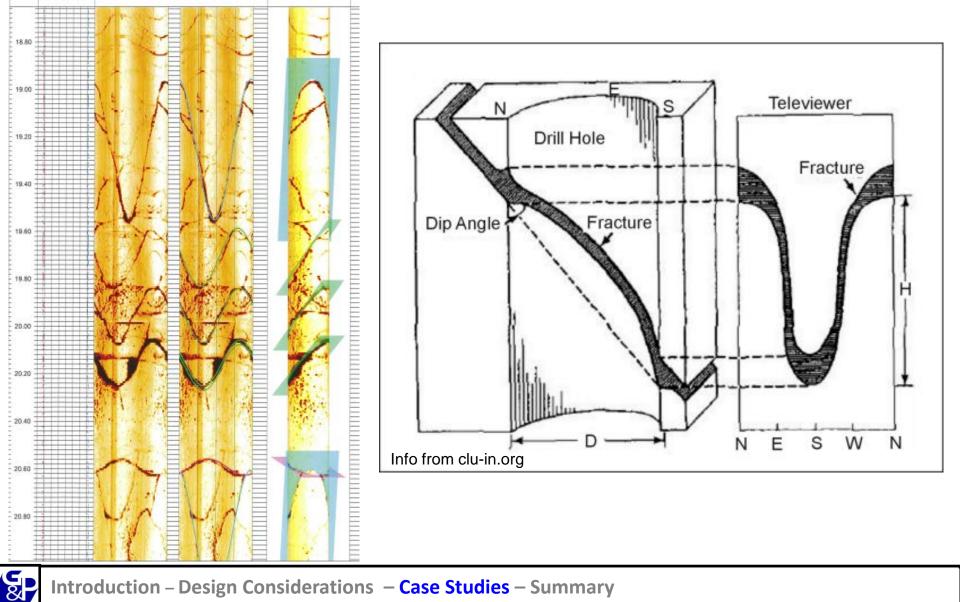
# BOREHOLE TELEVIEWER

Borehole Televiewer - Ultrasonic logging device

Radially mounted rotating transducer to scan borehole wall – Identify dip, fractures, bedding, etc.



# **BOREHOLE TELEVIEWER**



### **Maluri Portal**

Table 2. Partial load factors.

Load case	EL	DL	LL	TL	IL
Working condition	1.4	1.4	1.6	1.2	NA
Accidental impact	1.05	1.05	0.5	NA	1.05
One-strut failure	1.05	1.05	0.5	NA	NA

Note:

- EL Earth pressure and groundwater
- DL Dead load
- LL Live load
- TL Tempreture effect
- IL Accidental impact load
- NA Not applicable





### Steel Decking for the Traffic diversion above @ Maluri



8





# **Conchrane Station (Excavation Stage)** January 2013

### Conchrane Station (Launching of 2<sup>nd</sup> TBM)



### **Case History 2:**

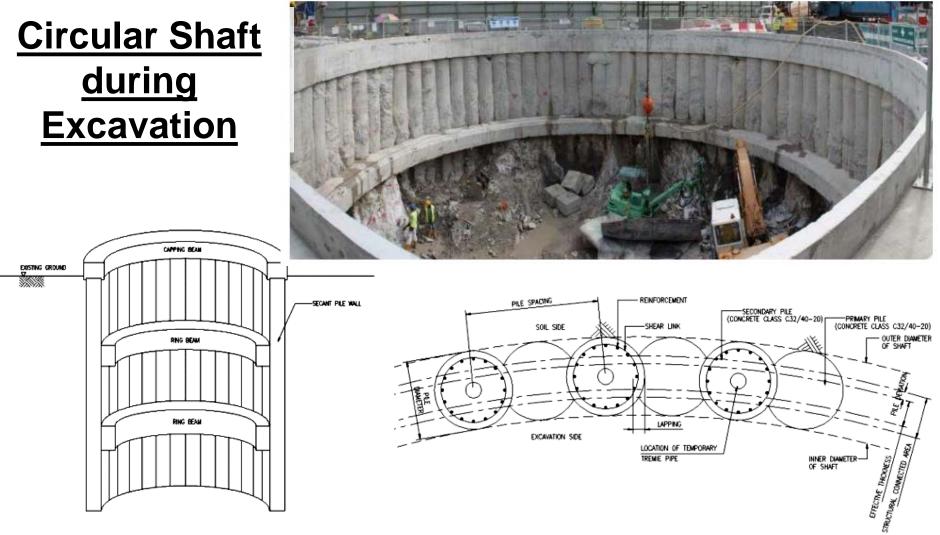
# **Circular Shaft for Launching of TBM in Kuala Lumpur**

# - KVMRT Line 1, Sungai Buloh to Kajang

### **Circular TBM Launching Shaft**



SP/



Sectional view of circular shaft with ring beams.



### **Design Based on Hoop Force**

 $Allowable \ compressive \ stress \ of \ concrete \geq \frac{Critical \ hoop \ force \ in \ wall}{Effective \ thickness \ of \ wall}$ 

where

Critical hoop force (kN per meter)

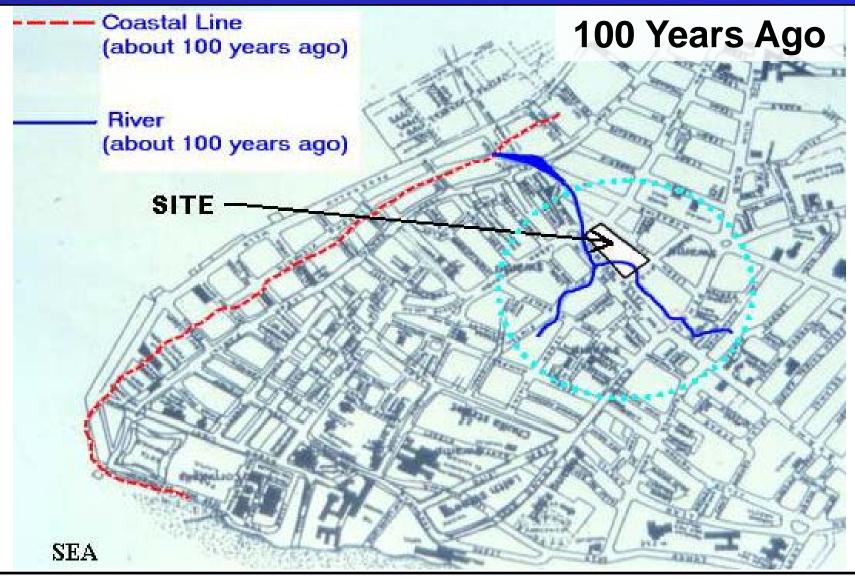
= (Maximum lateral pressure) x (0.5 of circular shaft outer diameter)

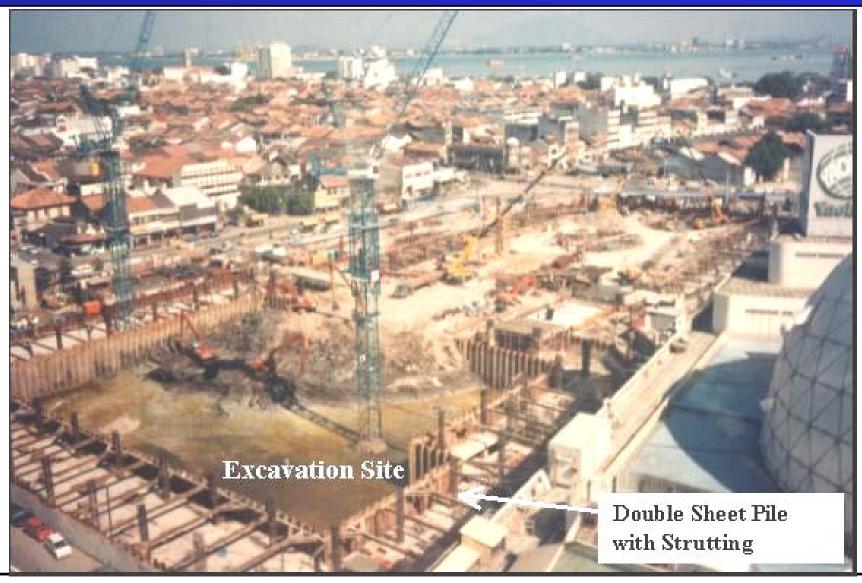
Effective thickness (m)

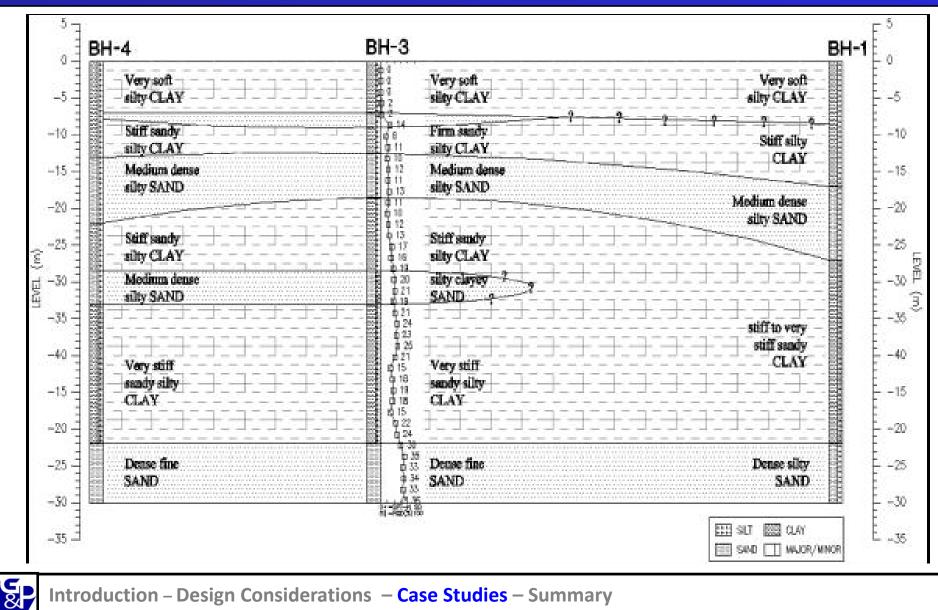
= (structurally connected area of retaining wall) – (pile deviation and verticality at critical depth during installation)

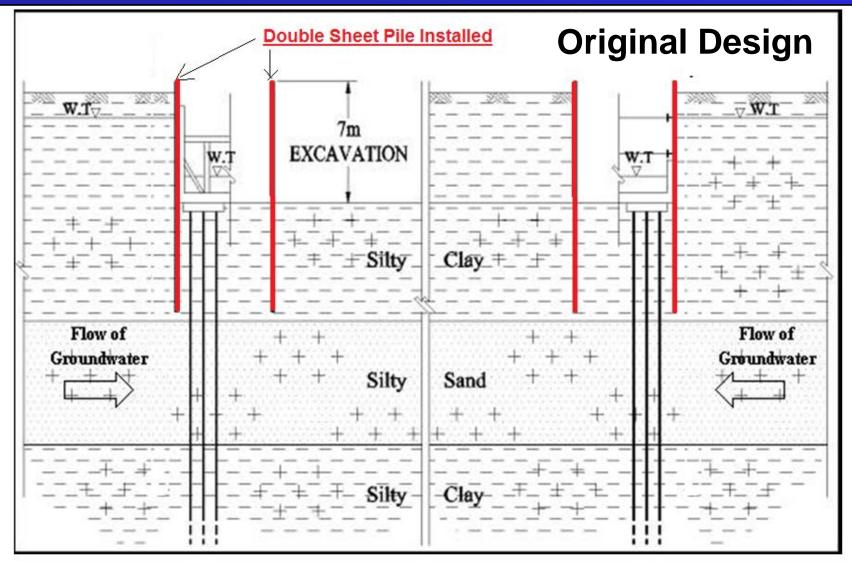
Allowable compressive stress of concrete (kPa) = 0.25 of concrete design strength

# **Case History 3:** Hydraulic Failure @ Penang in Alluvium with High Ground Water Table

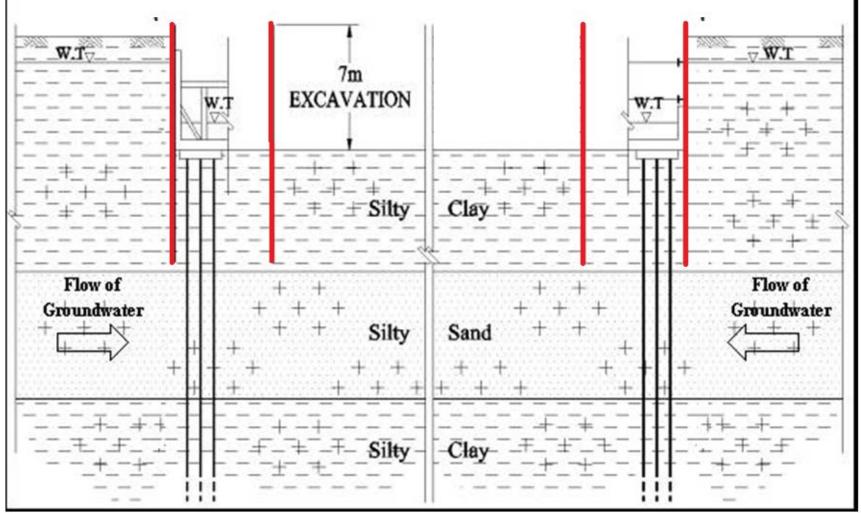






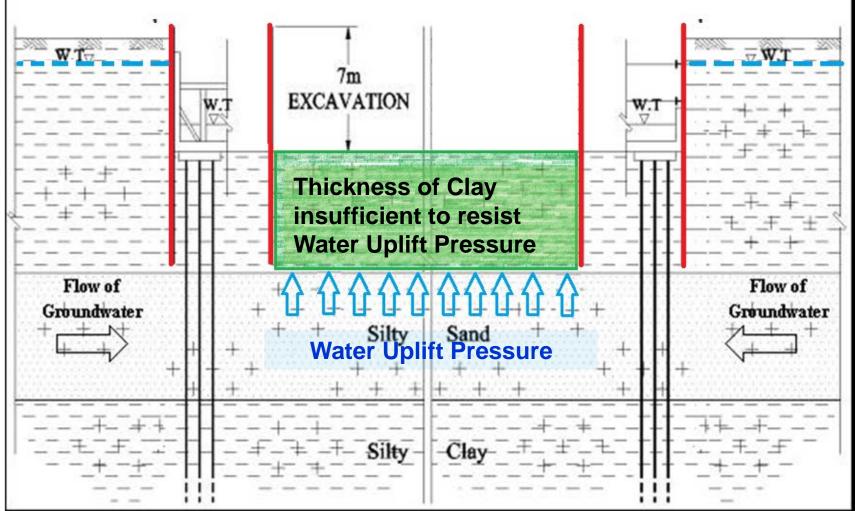


### **Original Retaining Wall (Insufficient Depth)**



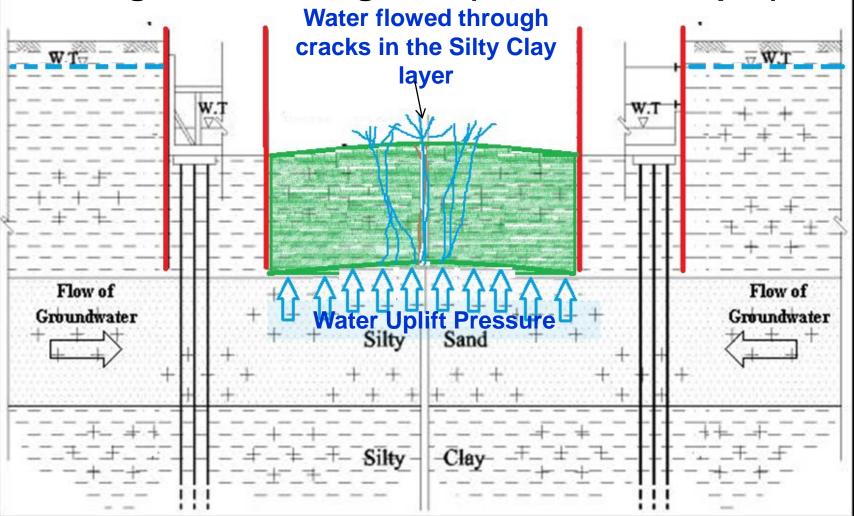


### **Original Retaining Wall (Insufficient Depth)**



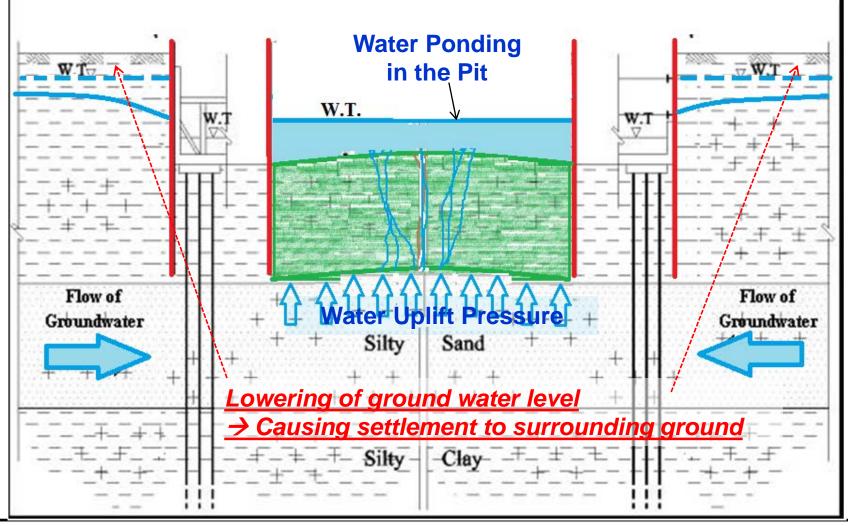


### **Original Retaining Wall (Insufficient Depth)**

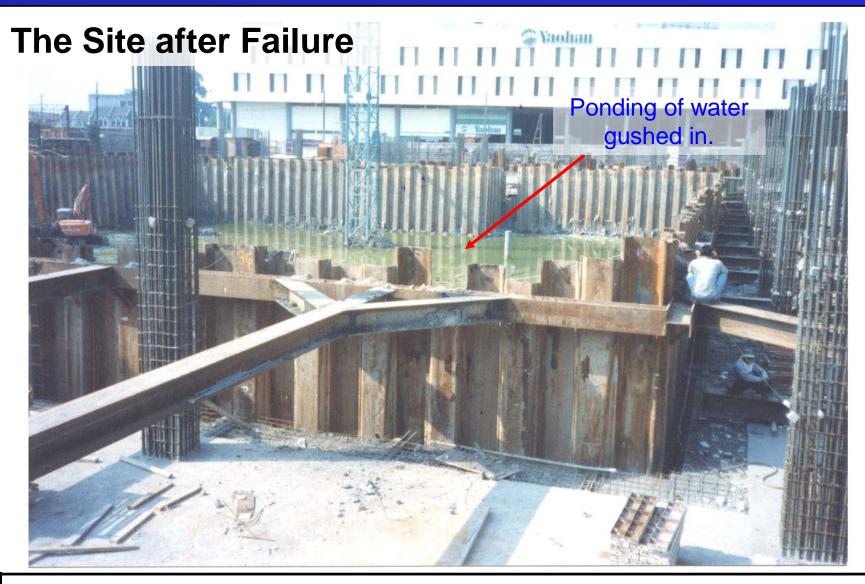




### **Original Retaining Wall (Insufficient Depth)**



SP-



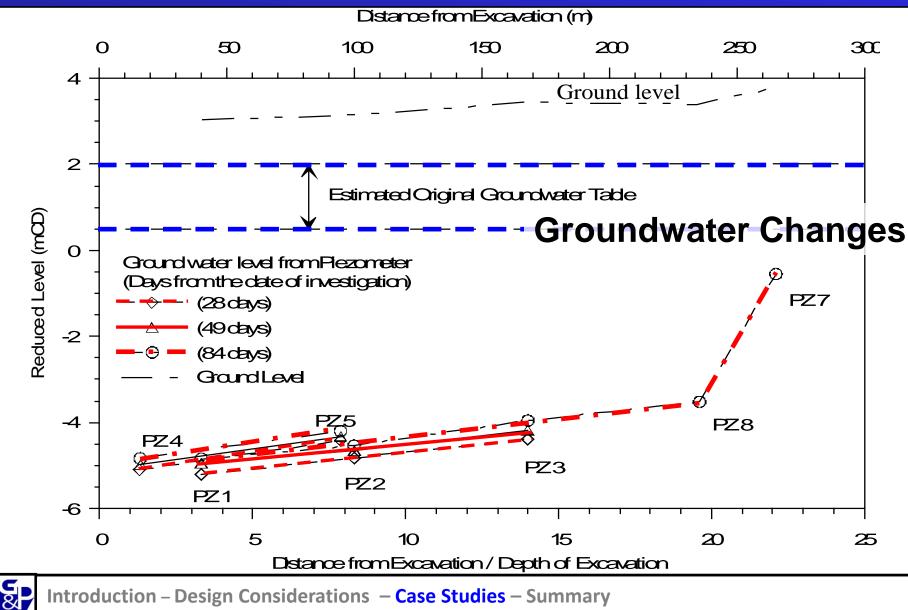


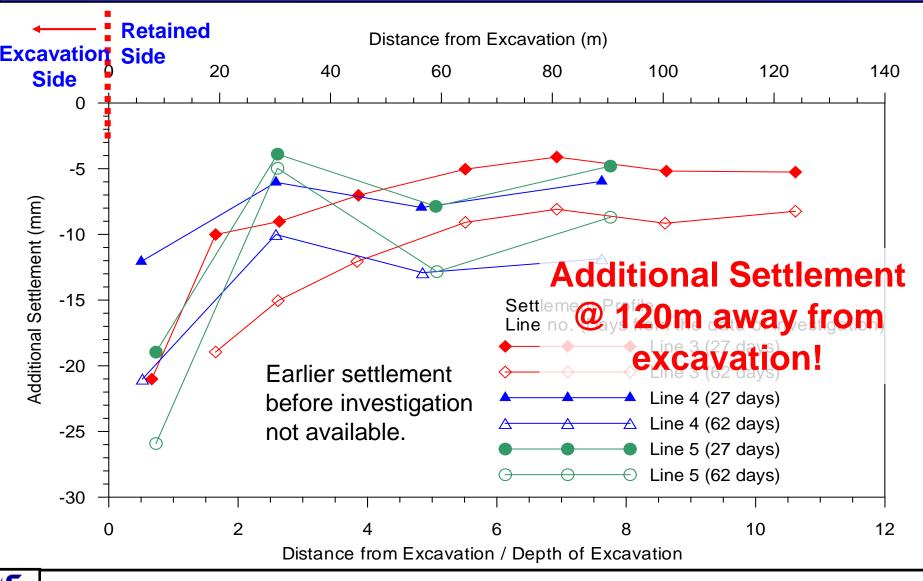
### Cracks of Houses – about 120 m away excavation

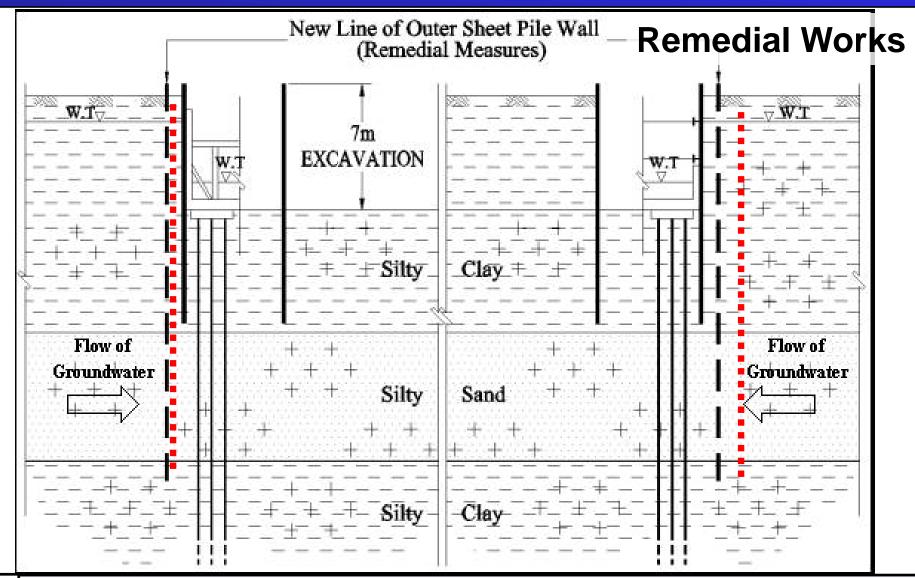










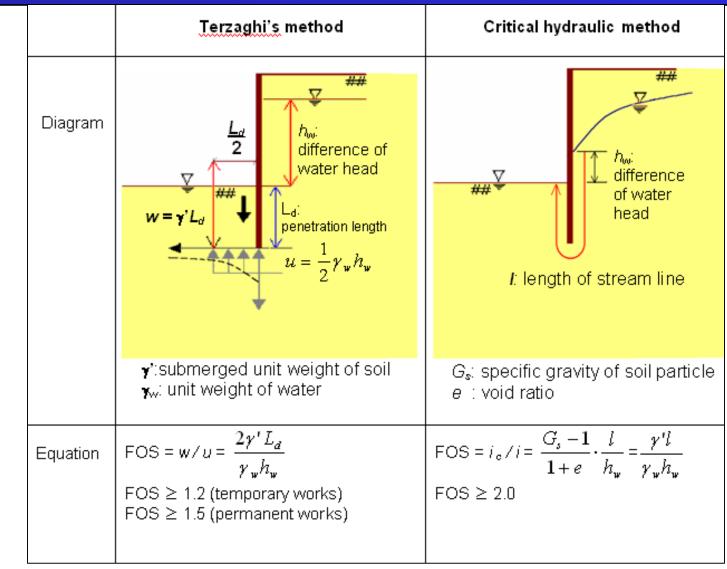


SP/

### **Hydraulic Failure**

- Base instability caused by piping
   Seepage due to high groundwater level
- Available methods
  - Terzaghi's method
  - Critical hydraulic gradient method

Hydraulic Failure Checks

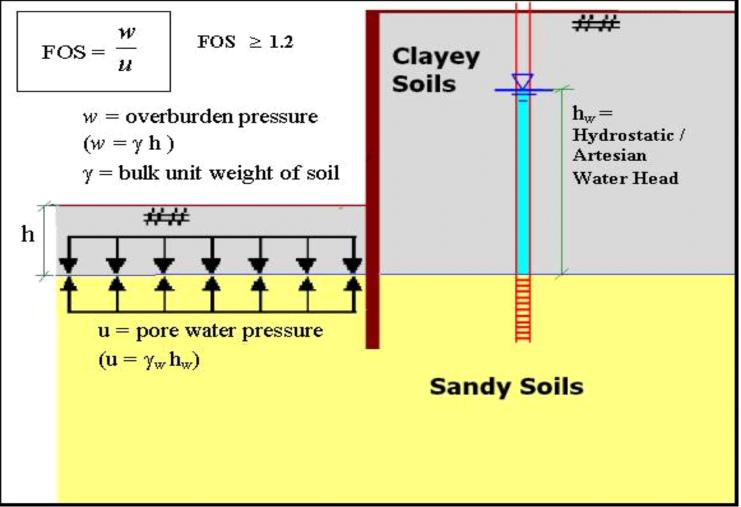




### **Hydraulic Failure**

- Terzaghi's method recommended
  - Based on latest research by Tanaka & Verruijt (1999)
  - Factor of safety required 1.2 to 1.5

### **HEAVING DUE TO ARTESIAN PRESSURE**



Introduction – Design Considerations – Case Studies – Summary

### **Hydraulic Failure**

- Heaving due to artesian pressure
  - Factor of safety 1.1 to 1.2
  - Smaller FOS sufficient as it did not consider shear strength or adhesion strength of the ground and retaining wall

### **Video of Hydraulic Failure**



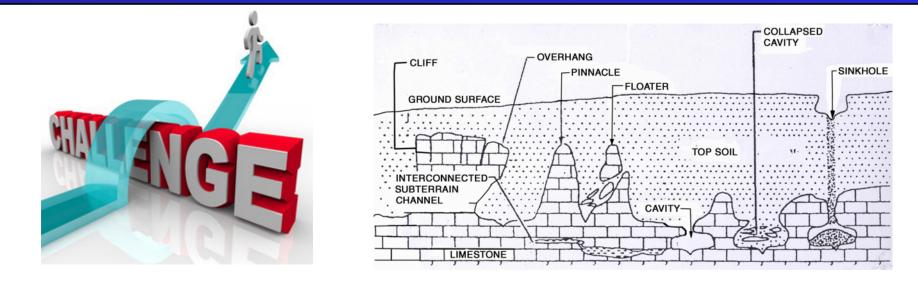






# Successful deep excavation depends on:

- Proper SI, Subsoil Profile, Parameters & calibrations
- Proper Constitutive models & Analyses
- Beware of Impact of Iowering water table & Mitigation measures



 Construction of deep excavation <u>in erratic</u> and complex Limestone formation requires multiple retaining systems and treatments together with strict control of vertical alignment with verification during construction



 Manage to use controlled blasting for the station construction with live traffic above the blasting level. The vibration is within the permissible limit of 25mm/s.





Cracks of Houses – about 120 m away excavation



 Deep excavation in Alluvium with sand layer lowered the water table to a distance of over 40 times the depth of excavation & induced settlements up to 120m away from excavation!



# ACKNOWLEDGMENT

The input from the following team members for KVMRT and in this presentation are very much appreciated:-

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- TIONG Chiong Ngu
- Ir. Dr. GUE Chang Shin
- Dr. GUE Chang Ye



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